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# POOR MAN'S INTRO TO BONDING

KICON ASIA 2025



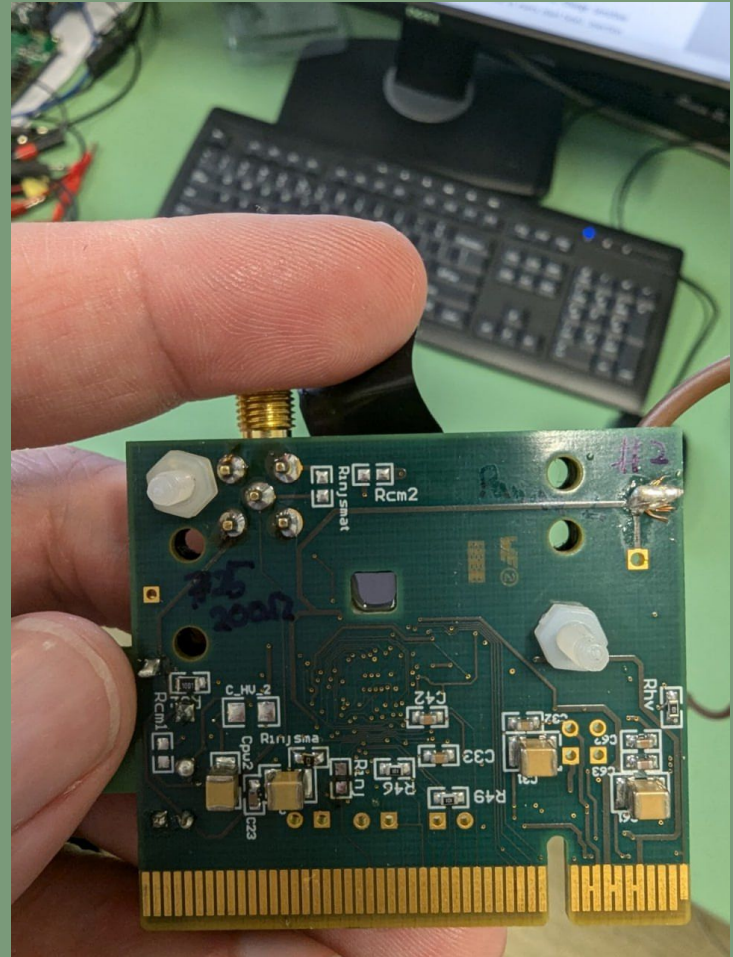
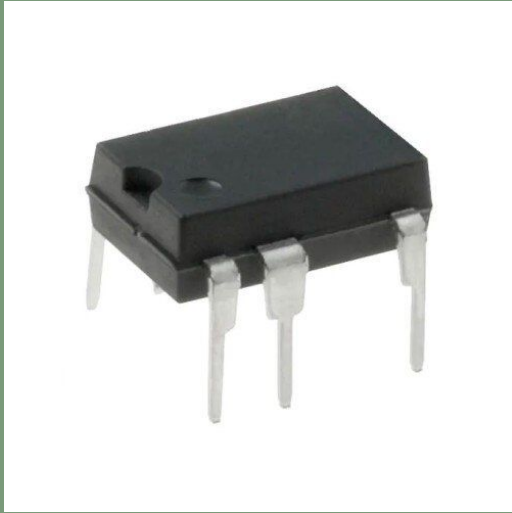
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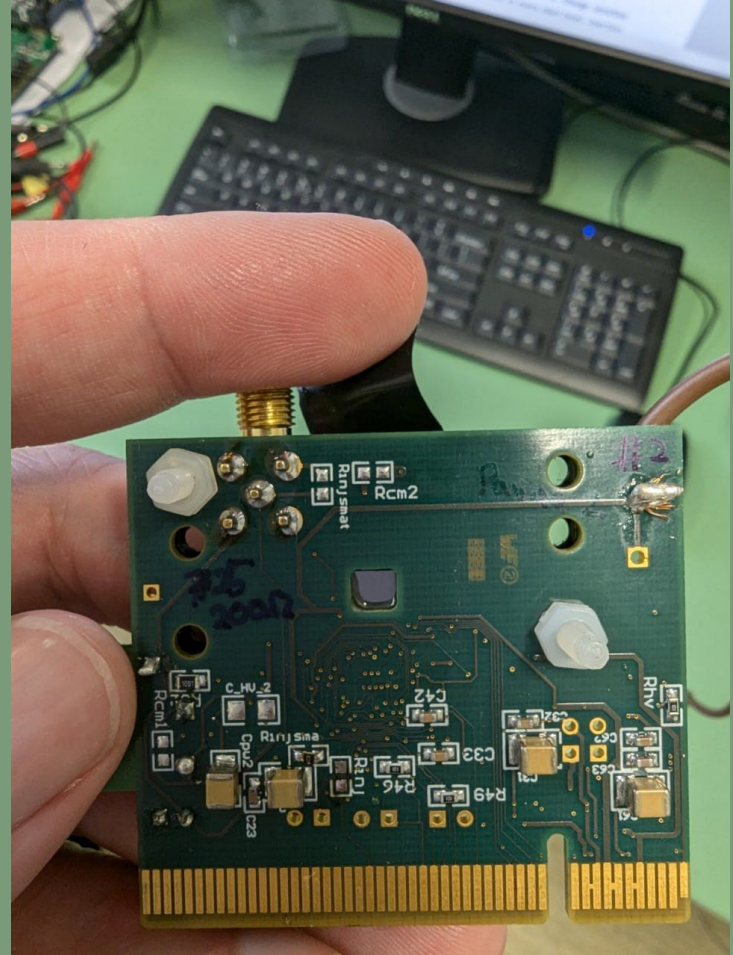
CONNECTING ENGINEERS AND  
UNIVERSITIES

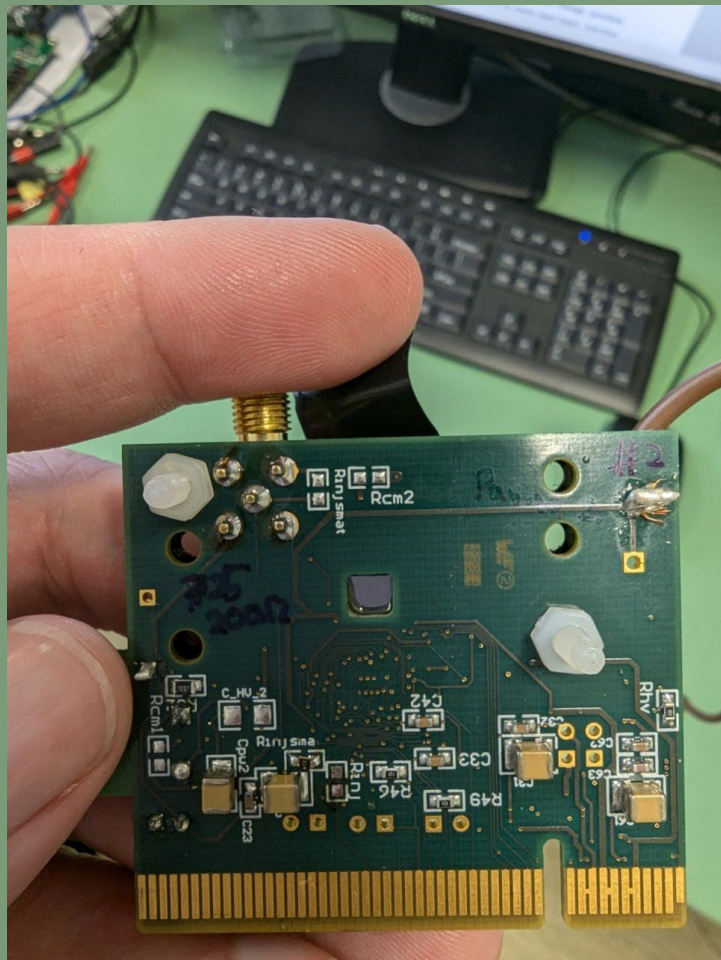
RUNNING CONFERENCES

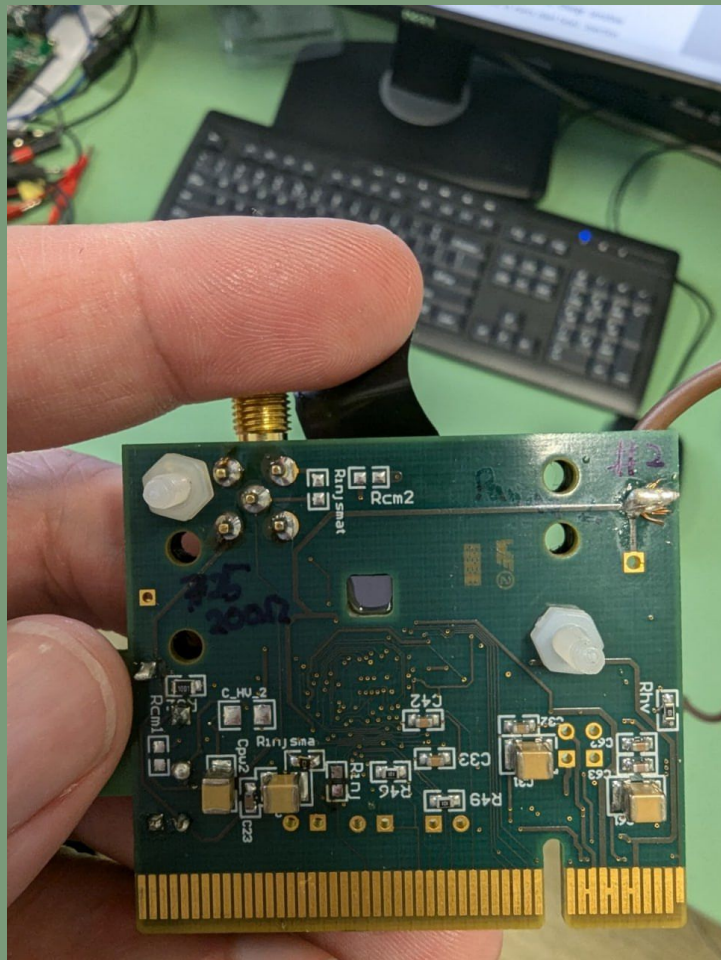
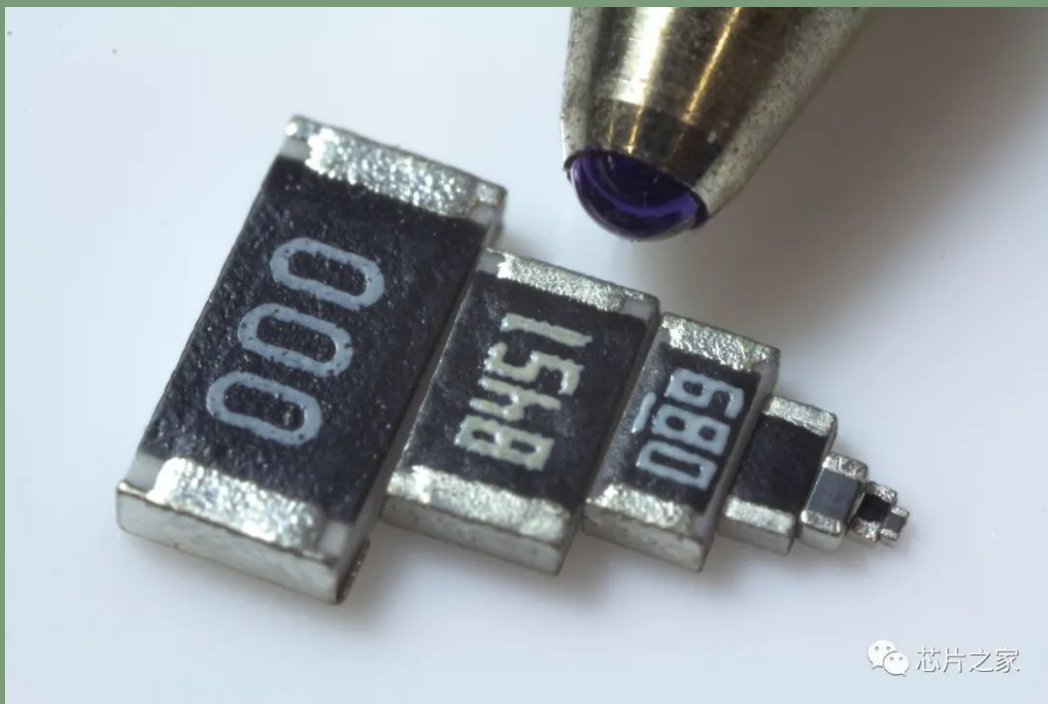
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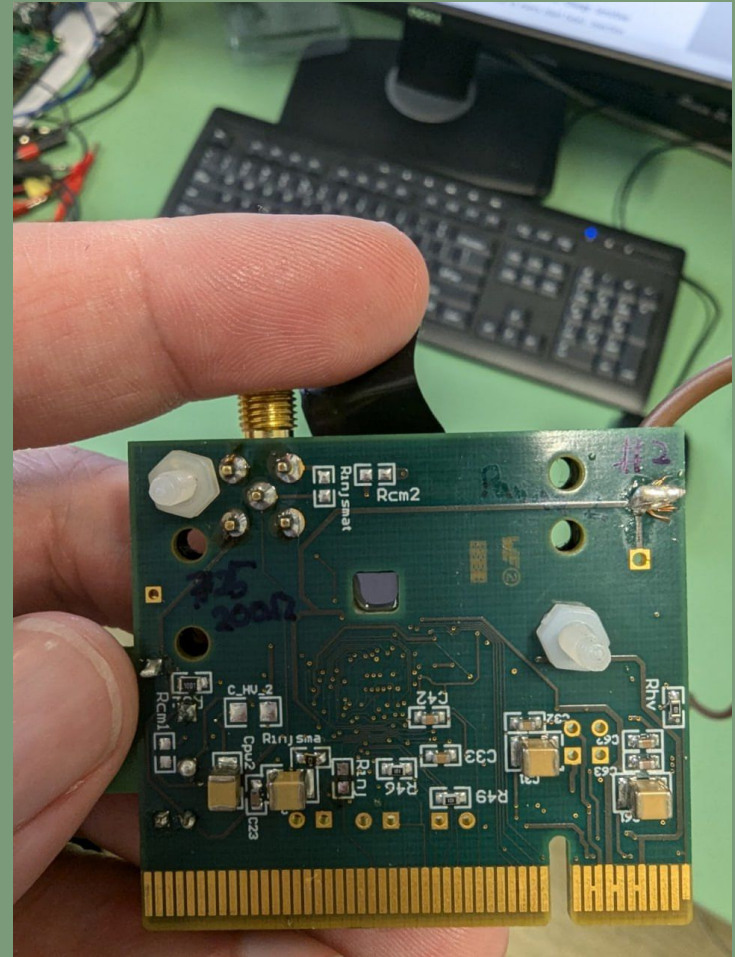
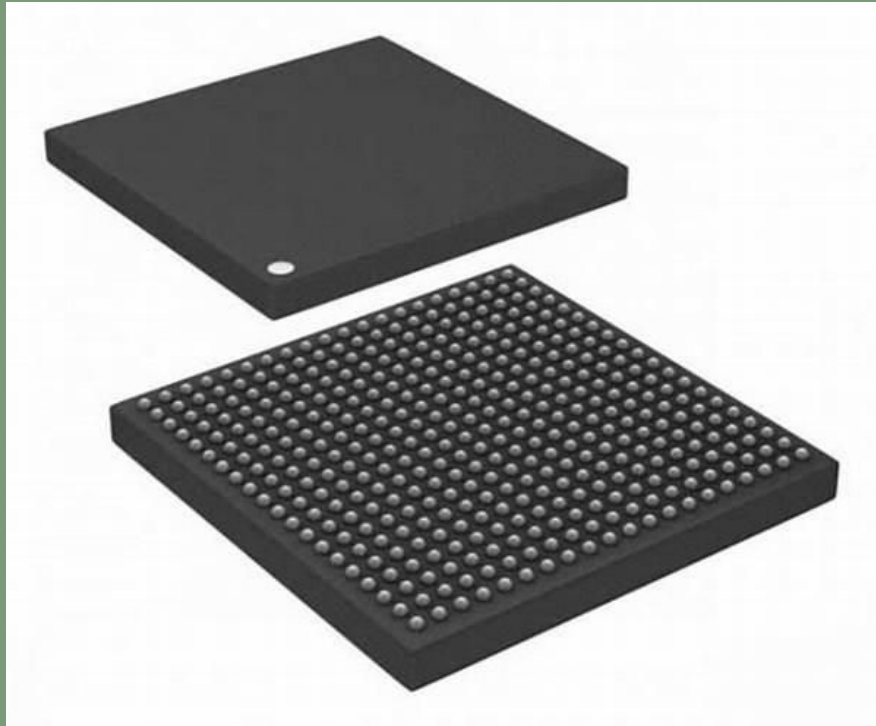


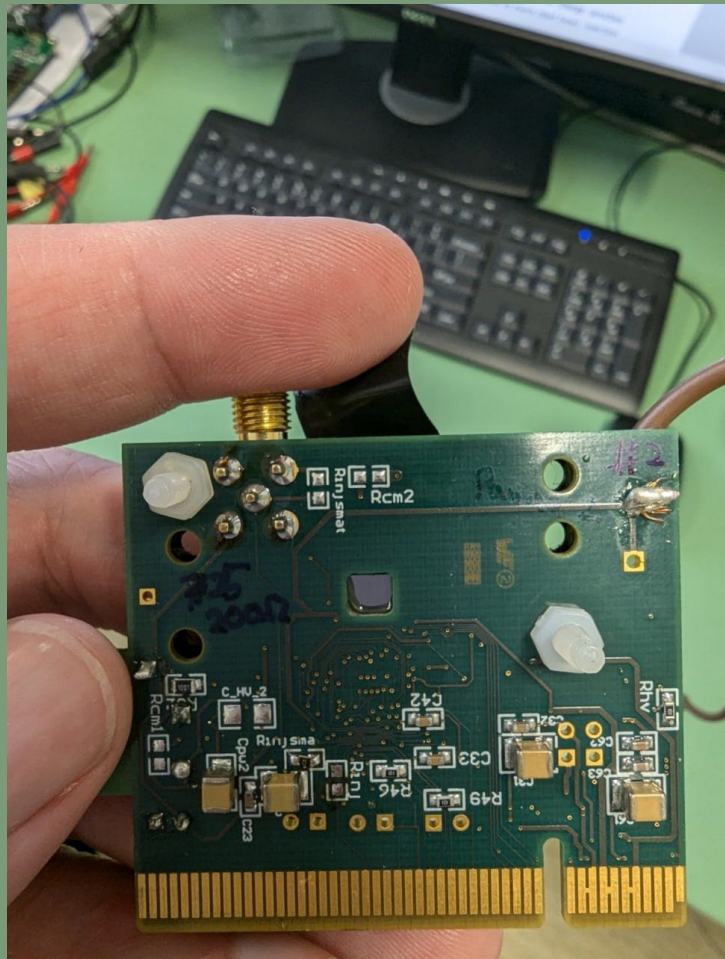
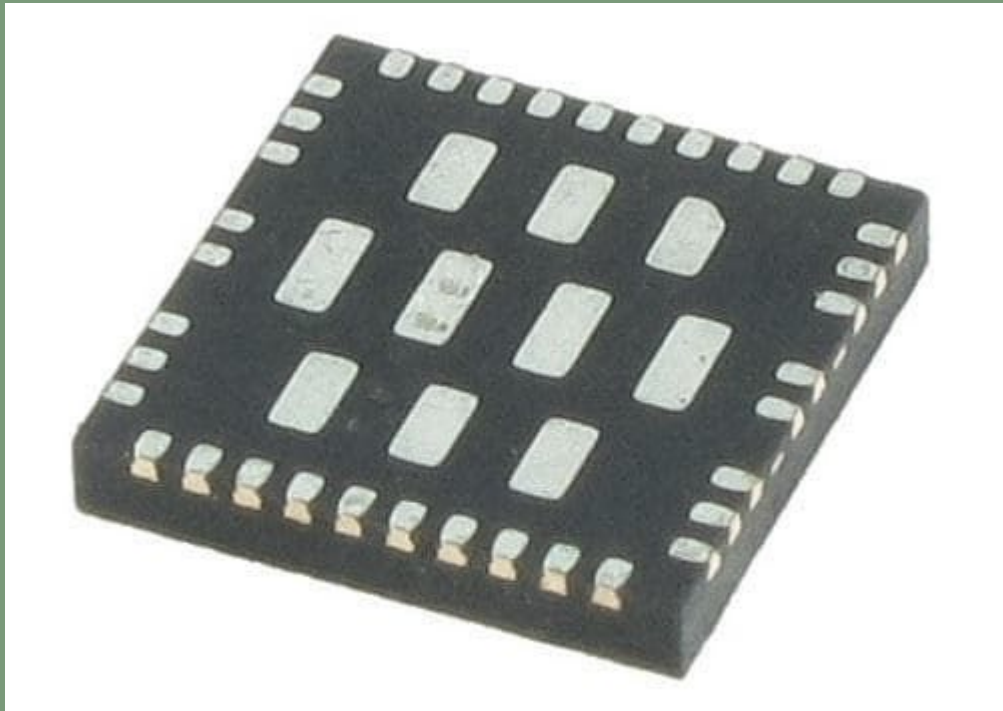


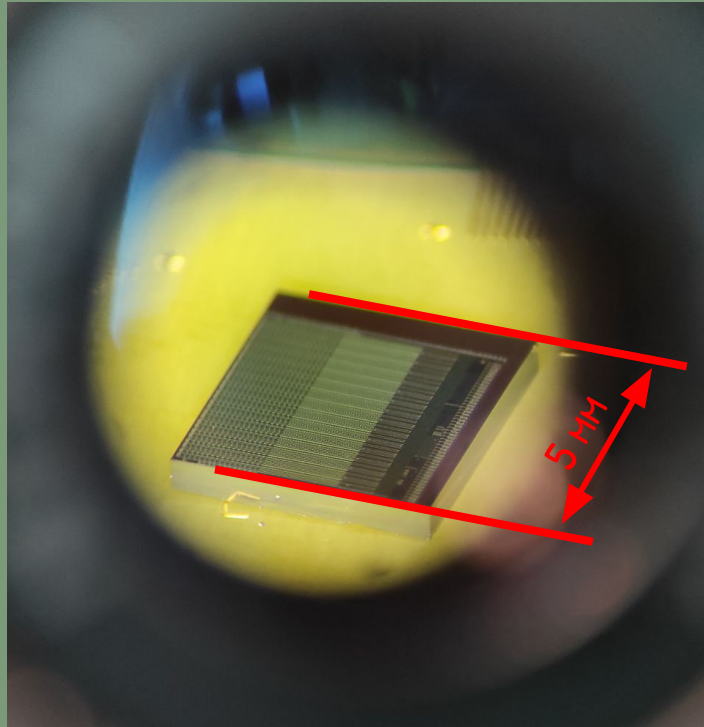




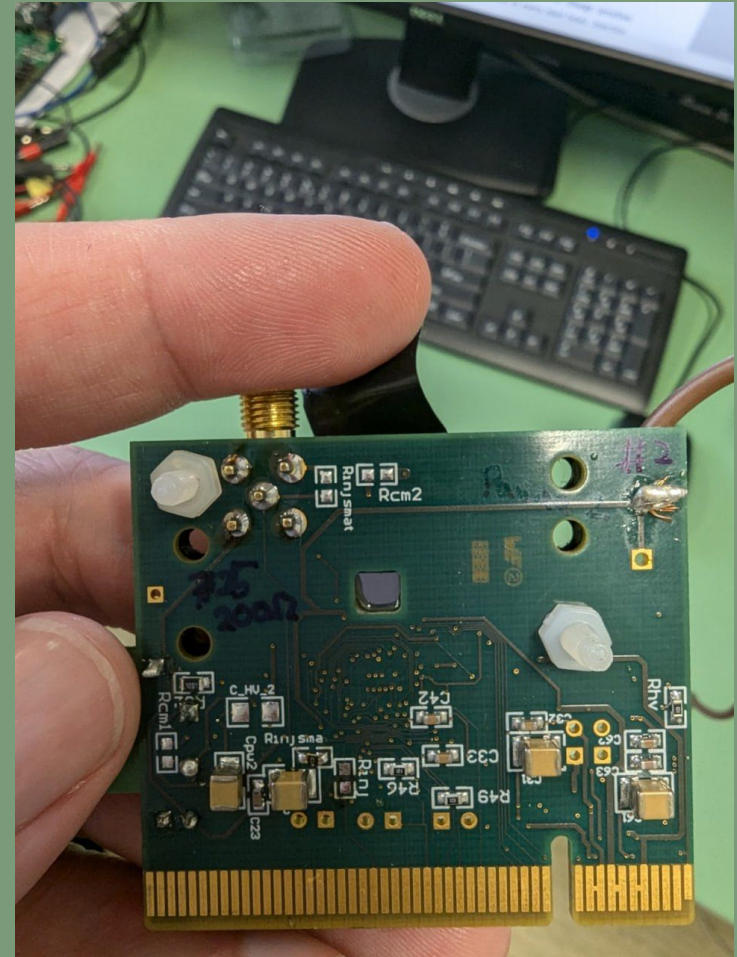


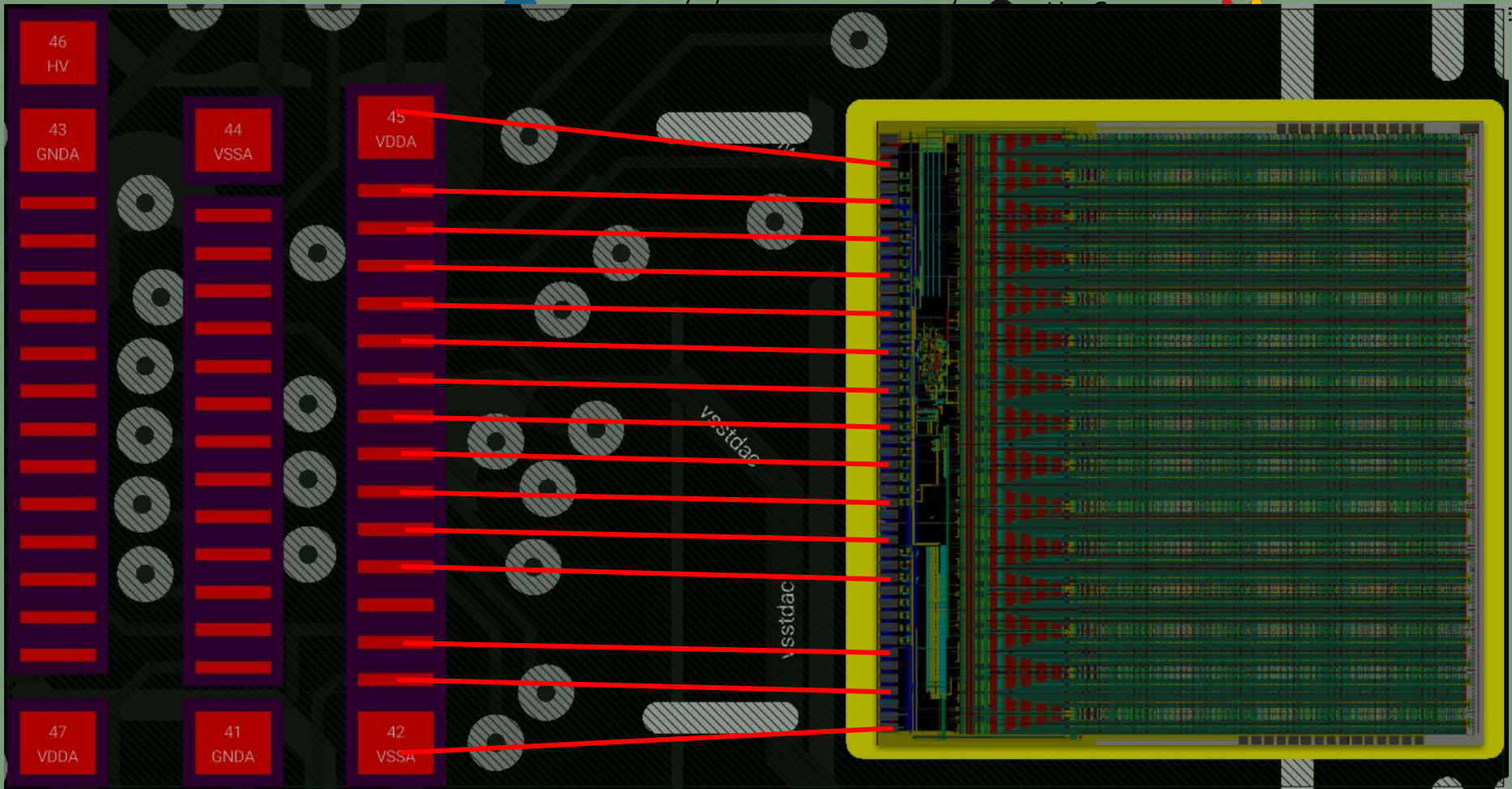






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HV

43  
GNDA

44  
VSSA

45  
VDDA

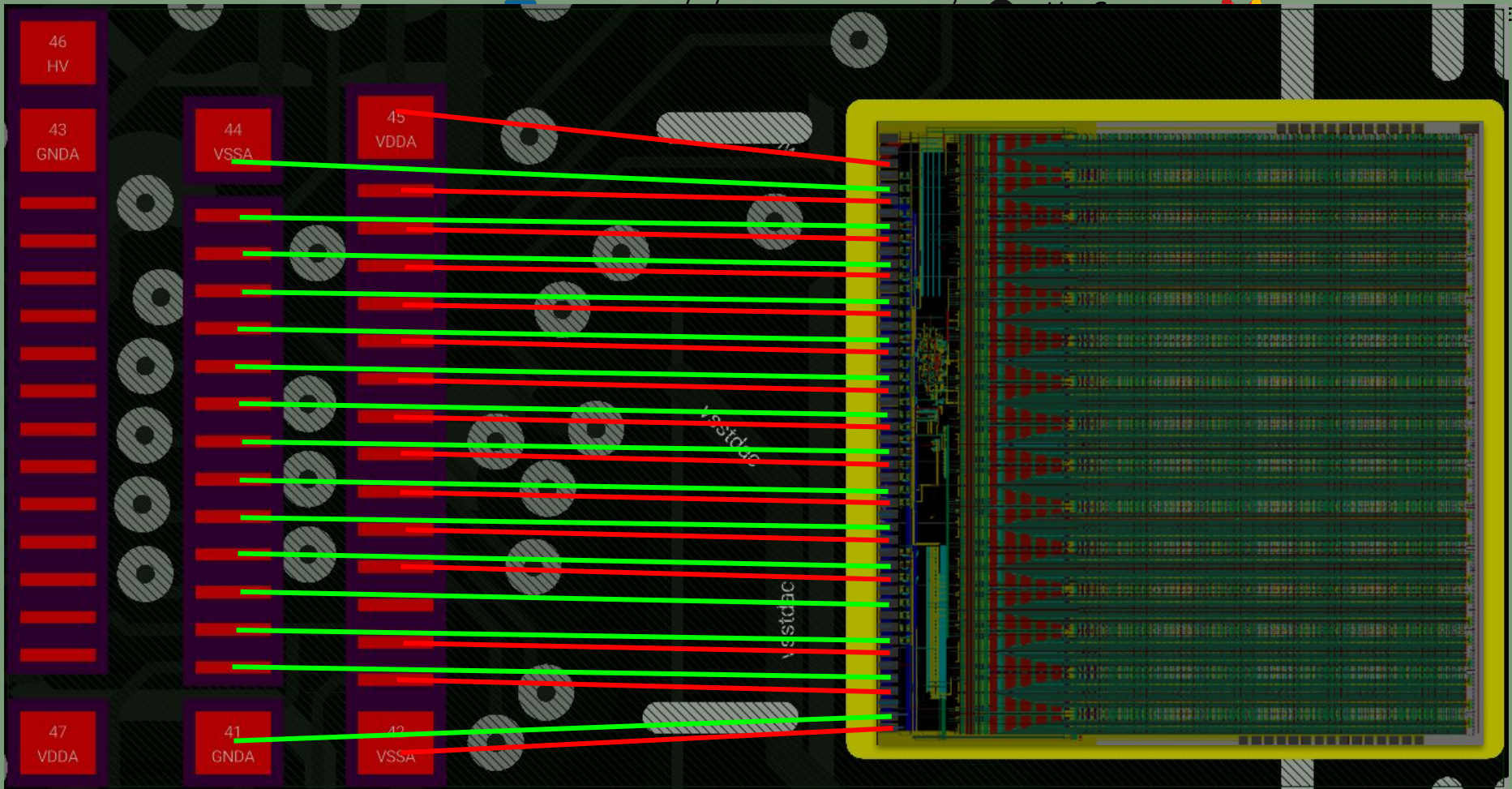
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VDDA

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VSSA

vsstdac

vsstdac



46  
HV

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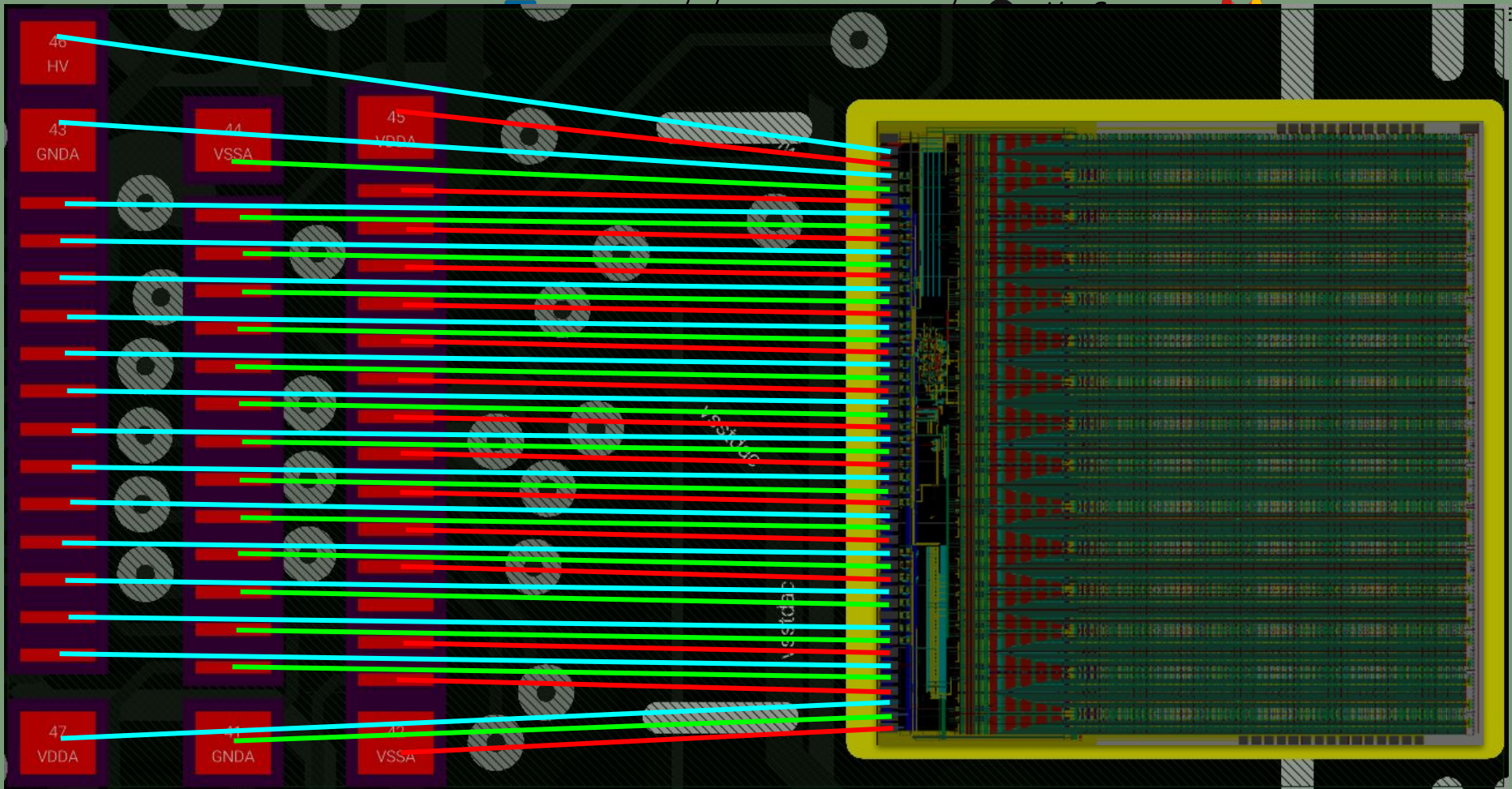
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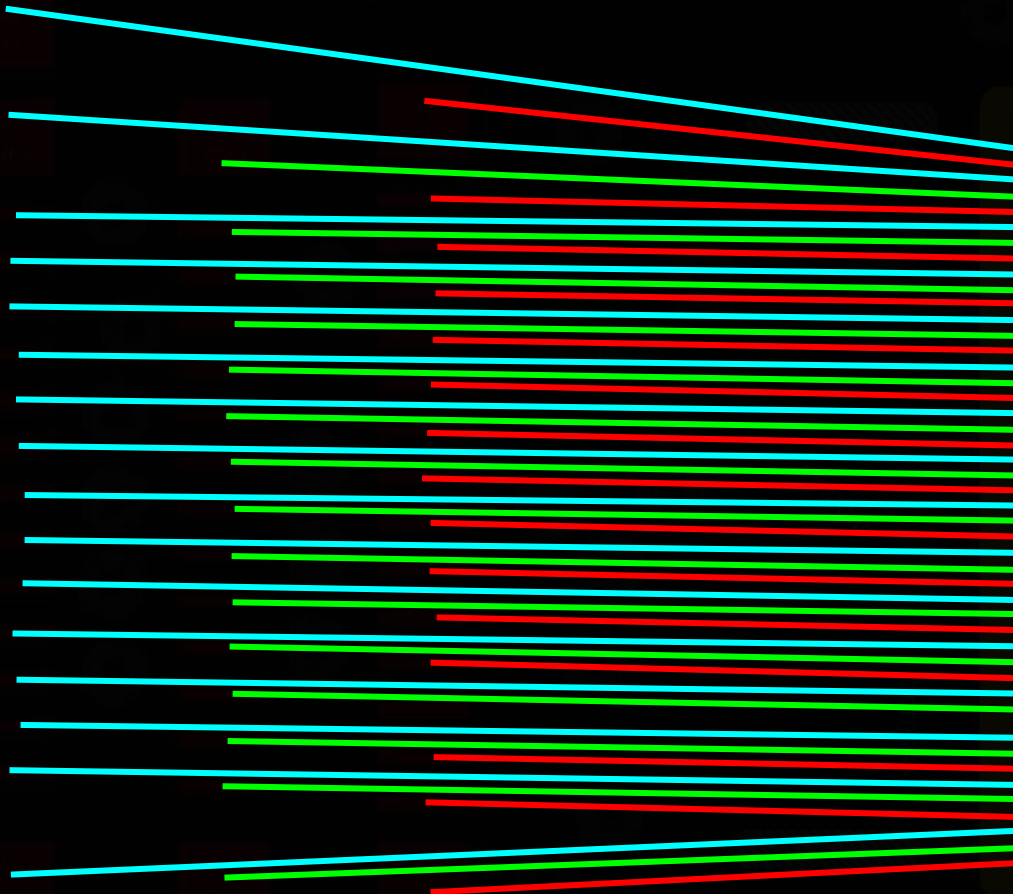
41  
GNDA

42  
VSSA

vstddac

vstddac





SubI	(pixels) -60V min
SubI	(chip ring) -60V min
VdataI	Analog power 1V8
Gndal	Analog Ground
VssaI	Analog power for the input PMOS of pxt-amp 1V2
Vnwell	pxt nwell bias 1V8 to 2V8
Vpwell	pxt pwell bias -1V8 to 0V
Trpix	Threshold for the main comparator BLPix + 50mV
Trpix2	Threshold for the slow comparator BLPix + 50mV
BLPix	Base line voltage of the pxt CR filter 1V in pxt
Vcage2	PMOS cascode voltage in the pxt amp 0V8
Vminuspix	Source voltage for the pxt line driver 0V5 - 1V5
Ampout	Source follower output - amplifier output, connect 1k Ohm to Ground
Inj	Analog input injection signal
Hbout	Source follower output - hit bus, connect 1kOhm to Gnd
VddI	Digital power - 1V8
GndI	Digital Ground
Vss (TDAC)	Current drain for regulated cascode receiver - 0V3
DataOutP	Digital out, LVDS, data out connect 100 Ohm pull up
DataOutN	Digital out, LVDS, data out connect 100 Ohm pull up
VminusPD	Ground for pull down transistor 0V
ToVCO	VCO bias, connect 1k and 1n in series
NoToVCO	VCO bias, connect 1k and 1n in series
VHigh	Power for PLL 1V8
VLow	Ground for PLL 0V
CSOut	Digital out, CMOS 1V8, shift register interface
CRb	Digital in, CMOS 1V8, shift register interface
CSin	Digital in, CMOS 1V8, shift register interface
CLd	Digital in, CMOS 1V8, shift register interface
CCK2	Digital in, CMOS 1V8, shift register interface
CCK1	Digital in, CMOS 1V8, shift register interface
CKExtN	Digital in, LCDS, external clk (no termination)
CKExtP	Digital in, LCDS, external clk (no termination)
CKRefP	Digital in, LCDS, reference clk for PLL (no termination)
CKRefN	Digital in, LCDS, reference clk for PLL (no termination)
SyncResN	Digital in, LCDS, sync reset (on chip termination)
SyncResP	Digital in, LCDS, sync reset (on chip termination)
Res_n	Digital in, CMOS 1V8, async reset active 0
MISO	Digital out, CMOS 1V8, SPI
MOSI	Digital in, CMOS 1V8, SPI
CSB	Digital in, CMOS 1V8, SPI
SCk	Digital in, CMOS 1V8, SPI
Gate	Gate voltage for NMOS comparator 2V1
Tfine (thtdac)	Threshold for TDC 1V4
Vddram	Vdd for RAM cells (1V5 - 1V8)
VdataI	Analog power 1V8
Gndal	Analog ground
VssaI	Analog power for input PMOS of pxt amp 1V2

Pad-Width =  
80µm

Pad-Pitch =  
100µm

## DISCLAIMER:

FOR COMPARISON - MOST OPEN-SOURCE SKY130 CHIPS  
(TINY TAPEOUT, OPENLANE, EFABLESS SHUTTLES):

- → 80  $\mu\text{m}$  WIDTH, 200  $\mu\text{m}$  PITCH (RECOMMENDED)

100  $\mu\text{m}$  PITCH IS TIGHT BUT POSSIBLE WITH 18-25  $\mu\text{m}$  AL WIRE

AND A SKILLED OPERATOR - JUST NOT THE "NORMAL" OPEN-SOURCE CASE!

Pad-Width =  
80 $\mu\text{m}$

Pad-Pitch =  
100 $\mu\text{m}$





## WIRE BONDING – CONNECTING CHIPS TO ELECTRODES WITH FINE WIRES



ULTRASONIC WIRE-BONDING = SOLID-STATE WELDING PROCESS  
INTERCONNECT A FINE METALLIC WIRE (Au, Al, Cu) TO A BOND PAD.

THE TOOL APPLIES A FORCE AND TRANSMITS  
US-VIBRATIONS TO THE WIRE-SUBSTRATE INTERFACE.

US-ENERGY INDUCES LOCALIZED PLASTIC DEFORMATION AND  
SCRUBBING ACTION THAT BREAKS UP SURFACE,  
ENABLING DIRECT METAL-TO-METAL INTERDIFFUSION.

NON-THERMOACTIVATED ULTRASONIC WIRE-BONDING WORKS SOLELY  
THROUGH PRESSURE AND ULTRASONIC ENERGY.  
PARTICULARLY FOR ALUMINUM WIRE BONDING TO  
GOLD METALLIZATION IN TEMPERATURE-SENSITIVE DEVICES.



# THE WIRE-BONDER

UPWARDS OF \$150k (NEW & CNC-PROGRAMMABLE)

USED MANUAL BONDERS STARTING  
AS LOW AS \$25k

CLEANROOM OR CLEAN ROOM

MAIN INGREDIENTS

- CNC COMPUTER (FOR AUTOMATION)
- VISIBILITY (CAMERA AND MICROSCOPE)
- WIRE-FEED
- STAGE





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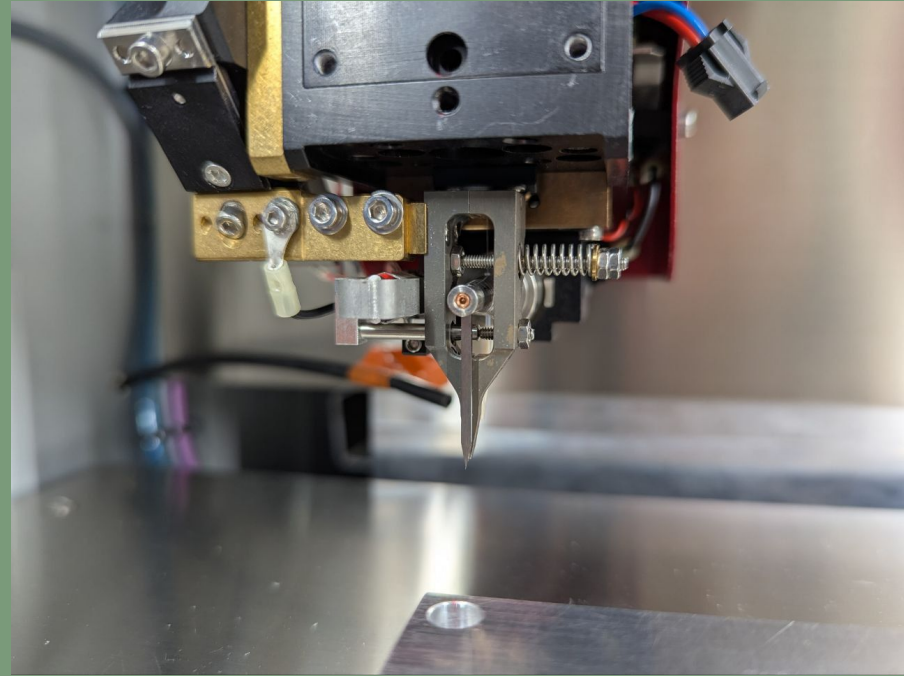
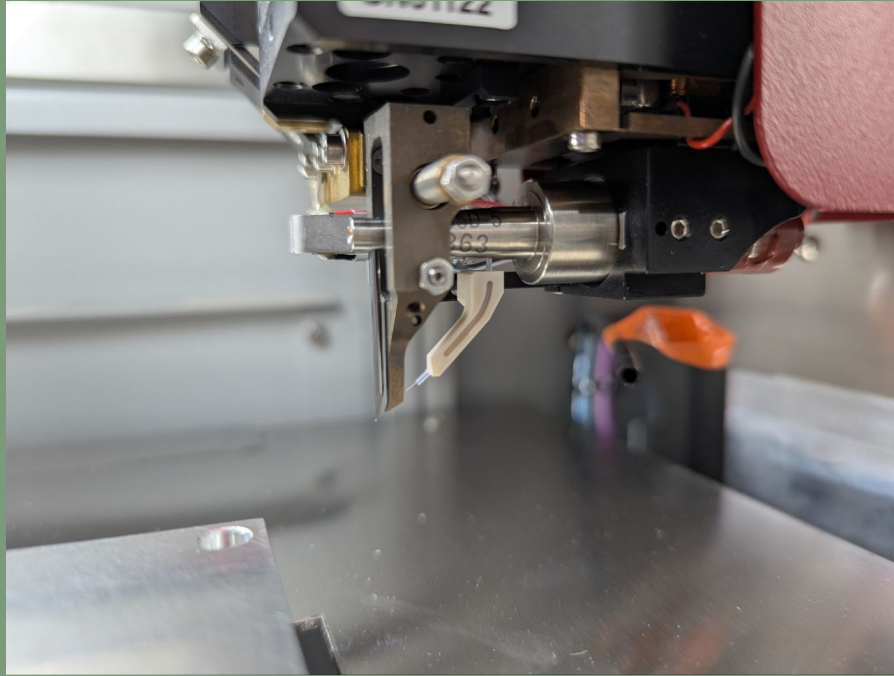
MAIN INGREDIENTS

- CNC COMPUTER (FOR AUTOMATION)
- VISIBILITY (CAMERA AND MICROSCOPE)
- WIRE-FEED
- STAGE
- BOND-HEAD + BOND-TOOL



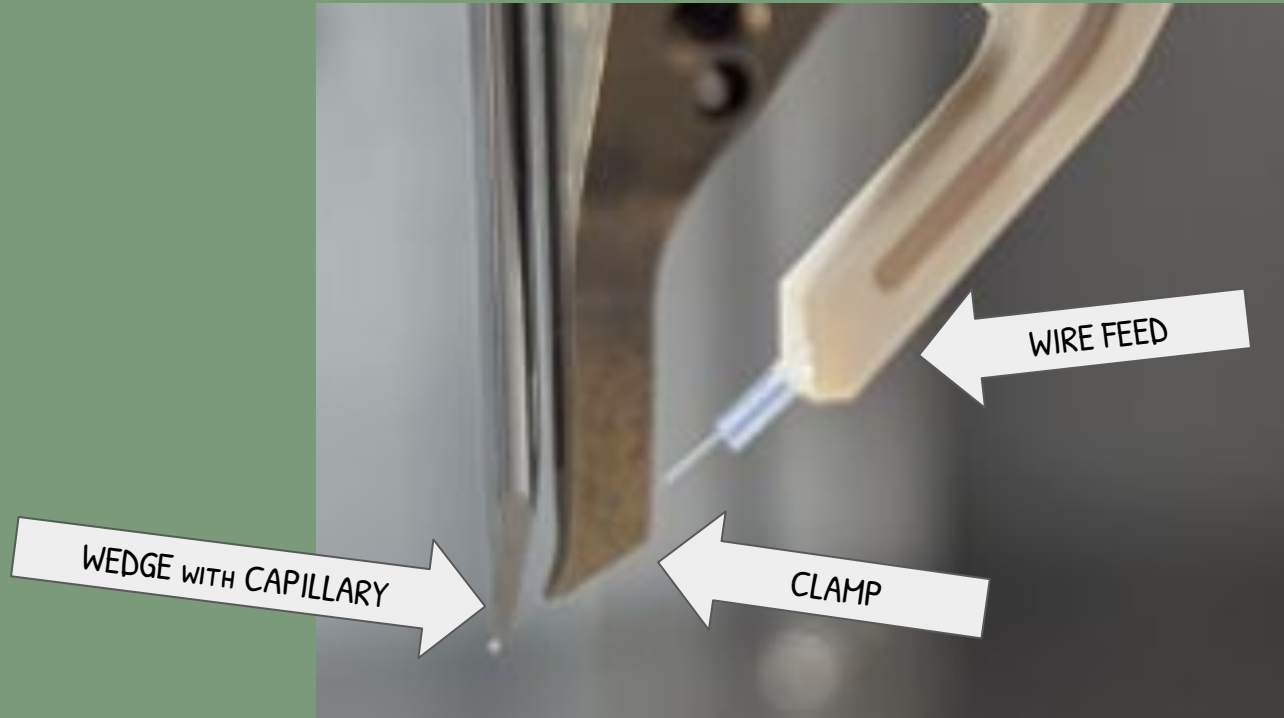


HEAD AND TOOL = WIRE-FEED + CLAMP + CAPILLARY + WEDGE





THE TOOL = WIRE-FEED + CLAMP + CAPILLARY + WEDGE



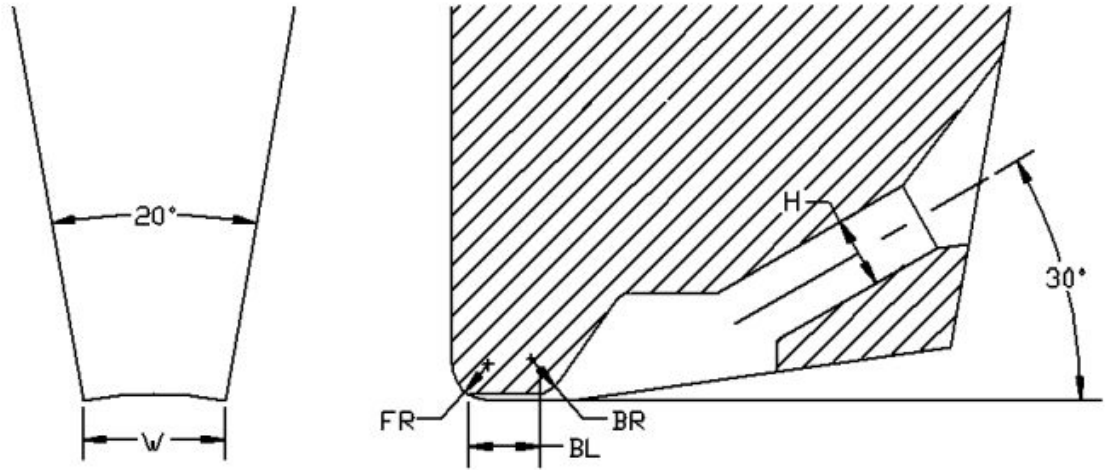


Figure 1: Schematic Diagram of the Wedge-shaped Capillary Cross-section.

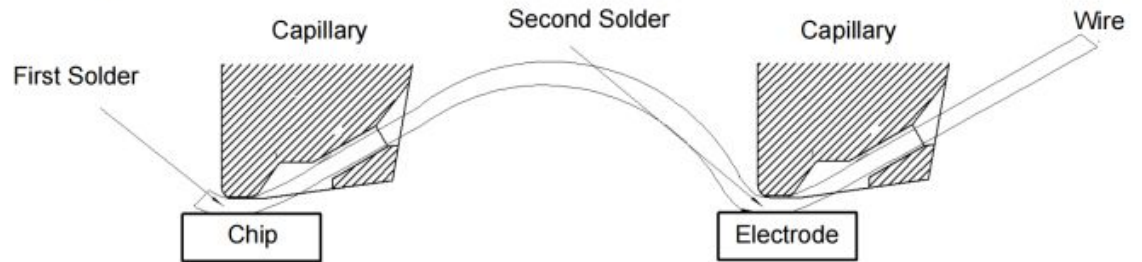


Figure 2: Schematic Diagram of Ultrasonic Wire Bonding.

BETTER VIEW OF THE WEDGE



INITIAL CONTACT

SCRUBBING

DEFORMATION

ATOMIC BONDING / INTERDIFFUSION

INTERMETALLIC COMPOUND

TEMPERING

FORM THE LOOP

SAME AGAIN

TEAR OFF

# 9 SIMPLE STEPS



## INITIAL CONTACT

SCRUBBING

DEFORMATION

ATOMIC BONDING / INTERDIFFUSION

INTERMETALLIC COMPOUND

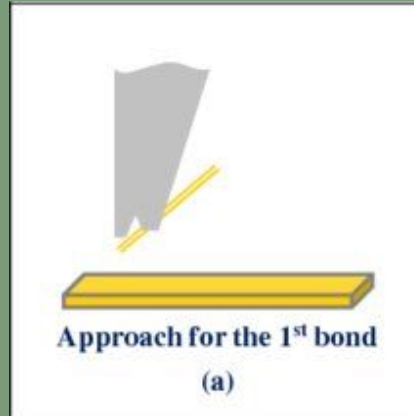
TEMPERING

FORM THE LOOP

SAME AGAIN

TEAR OFF

- SURFACE APPROACHES.
- ELECTRODES POSITION WIRE, SUBSTRATE REMAINS STABLE.
- MECHANICAL FORCE ESTABLISHES INITIAL INTIMATE CONTACT.
- ON CONTACT: PRESSURE BUILDS, ALIGNMENT BEGINS.
- ENERGY FOCUSES ACROSS MINUSCULE BONDING ZONE.
- WIRE CONFORMS, ADAPTING TO TARGET SURFACE.
- FOUNDATION FORMS FOR SUBSEQUENT METALLURGICAL PROCESSES.





INITIAL CONTACT

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DEFORMATION

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INTERMETALLIC COMPOUND

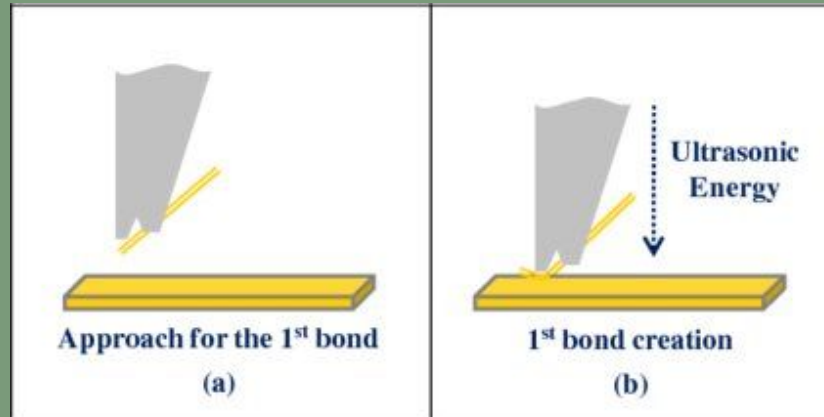
TEMPERING

FORM THE LOOP

SAME AGAIN

TEAR OFF

- ULTRASONIC VIBRATION INITIATES MICRO-SCALE SCRUBBING (60-140kHz).
- LOCALIZED RELATIVE MOTION DISRUPTS RESIDUAL INTERFACIAL BARRIERS.
- REMOVES OXIDES AND CONTAMINANTS.
- SURFACE ASPERITIES BREAK, EXPOSING CLEAN METAL.
- FRICTIONAL ENERGY ENHANCES ATOMIC MOBILITY SIGNIFICANTLY.
  - INTRODUCING LATTICE DEFECTS
  - SIGNIFICANT HEAT IN ATTOLITER VOLUME ( $>800^{\circ}\text{C}$ )
- SCRUBBING ESTABLISHES CONTACT CONDITIONS RELIABLY.



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INTERMETALLIC COMPOUND

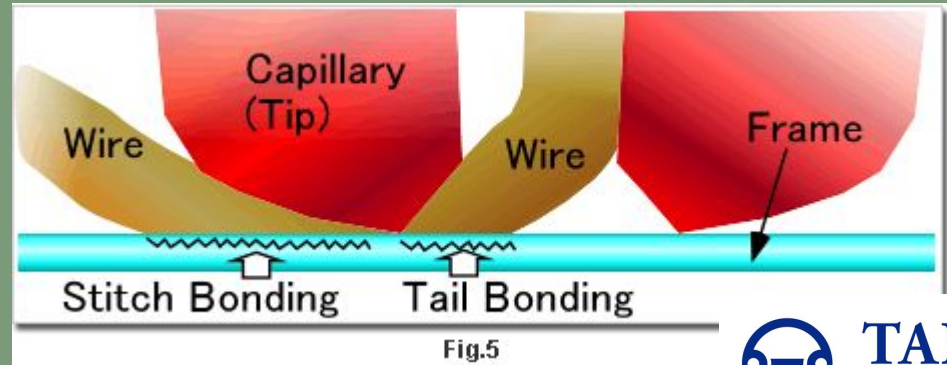
TEMPERING

FORM THE LOOP

SAME AGAIN

TEAR OFF

- APPLIED FORCE RESHAPES WIRE UNDER STRESS.
- PLASTIC FLOW ACCOMMODATES SURFACE IRREGULARITIES FULLY.
- WIRE FLATTENS, ENLARGING CONTACT AREA GRADUALLY.
- MECHANICAL SHAPING SUPPORTS STRONGER ATOMIC COUPLING.
- INTERFACES COMPRESS, REDUCING INTERFACIAL VOIDS.
- DEFORMATION PREPARES PATHWAY FOR INTERDIFFUSION PHENOMENA.



**TANAKA**  
TANAKA PRECIOUS METALS

INITIAL CONTACT

SCRUBBING

DEFORMATION

ATOMIC BONDING / INTERDIFFUSION

INTERMETALLIC COMPOUND

TEMPERING

FORM THE LOOP

SAME AGAIN

TEAR OFF

- CLEAN METALLIC ATOMS ENCOUNTER NEIGHBORING ATOMS.
- DIFFUSION INITIATES ACROSS FRESHLY ACTIVATED INTERFACE.
- ATOMIC PROXIMITY ALLOWS ELECTRONIC ORBITAL OVERLAP.
- GRADUAL INTERDIFFUSION INTEGRATES WIRE AND PAD.
- METALLURGICAL COHESION STRENGTHENS MECHANICAL BOND INTEGRITY.
- ATOMIC ATTRACTION CONSOLIDATES IRREVERSIBLE METALLURGICAL JUNCTION.

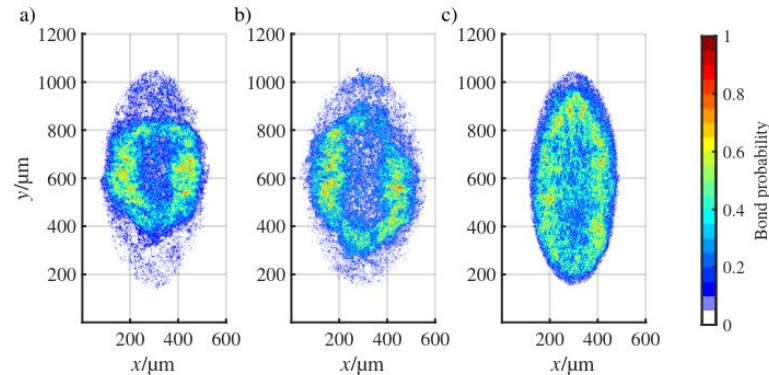


Figure 3.29: Results of image segmentation at 10,000 oscillation cycles of 15 pealed interface images for a) 37 kHz, b) 60 kHz and c) 100 kHz.

INITIAL CONTACT

SCRUBBING

DEFORMATION

ATOMIC BONDING / INTERDIFFUSION

INTERMETALLIC COMPOUND

TEMPERING

FORM THE LOOP

SAME AGAIN

TEAR OFF

- DISTINCT PHASES FORM BETWEEN CONTACTING METALS.
- IMC NUCLEATE AT BONDING INTERFACE.
- GROWTH DEPENDS ON TEMPERATURE, TIME, CHEMISTRY.
- THESE COMPOUNDS STABILIZE INITIAL METALLURGICAL CONNECTION.
- EXCESSIVE GROWTH RISKS BRITTLE JOINT FORMATION.
- CONTROLLED KINETICS ENSURE RELIABLE INTERMETALLIC STRUCTURE.

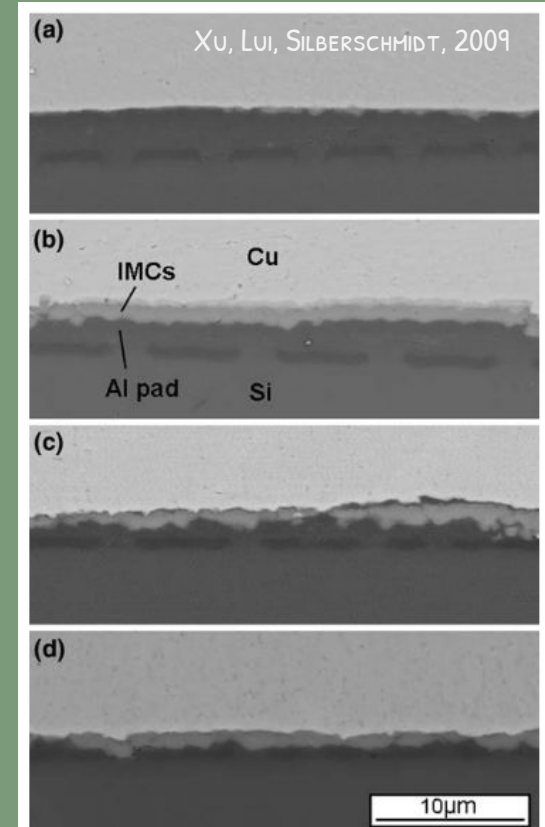


Fig. 6. Cross-sectional BSE SEM of copper ball/Al metallization interfaces after aging at 200°C for: (a) 1 day, very small IMCs formed; (b) 4 days, a layer of IMCs formed; (c) 64 days, thicker IMCs; and (d) 121 days, 1.5-µm-thick IMCs formed.



INITIAL CONTACT

SCRUBBING

DEFORMATION

ATOMIC BONDING / INTERDIFFUSION

INTERMETALLIC COMPOUND

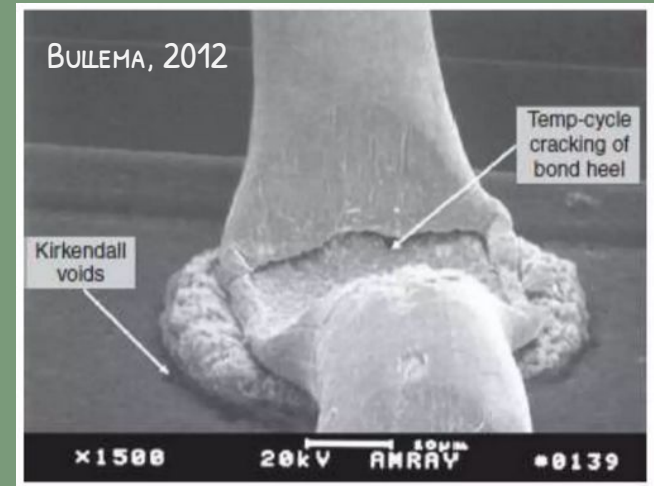
TEMPERING

FORM THE LOOP

SAME AGAIN

TEAR OFF

- OPTIONAL
- BOND UNDERGOES STRESS RELAXATION THROUGH TEMPERING.
- RESIDUAL MECHANICAL STRAIN GRADUALLY DISSIPATES INTERNALLY.
- HEAT ENHANCES MICROSTRUCTURAL STABILIZATION POST-BONDING.
- DIFFUSION BALANCES INTERFACIAL COMPOSITION MORE UNIFORMLY.
- BOND ACHIEVES GREATER TOUGHNESS AND RELIABILITY.





INITIAL CONTACT

SCRUBBING

DEFORMATION

ATOMIC BONDING / INTERDIFFUSION

INTERMETALLIC COMPOUND

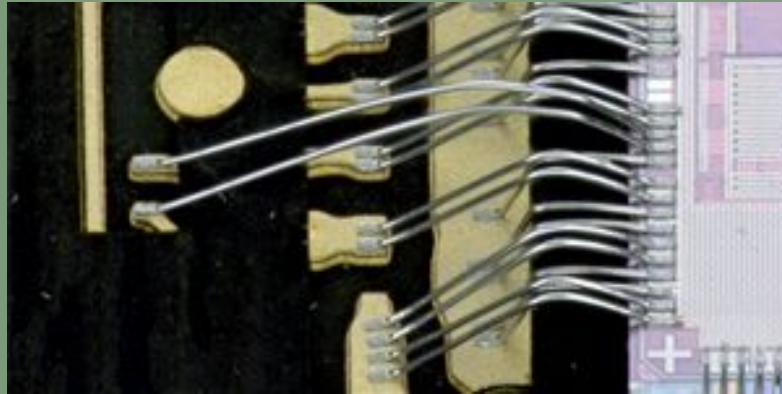
TEMPERING

FORM THE LOOP

SAME AGAIN

TEAR OFF

- CAPILLARY ASCENDS, WIRE FOLLOWS GUIDED TRAJECTORY.
- LOOP HEIGHT DETERMINED BY PROGRAMMED MACHINE PARAMETERS.
- ULTRASONIC VIBRATIONS CEASE DURING UPWARD FORMATION.
- WIRE BENDS SMOOTHLY, DEFINING ELECTRICAL INTERCONNECT.
- MECHANICAL PATH OPTIMIZES STRESS DISTRIBUTION EFFECTIVELY.
- LOOP GEOMETRY ENSURES FUNCTIONAL ELECTRICAL CONNECTION.





INITIAL CONTACT

SCRUBBING

DEFORMATION

ATOMIC BONDING / INTERDIFFUSION

INTERMETALLIC COMPOUND

TEMPERING

FORM THE LOOP

SAME AGAIN

TEAR OFF

- BONDING TOOL REPOSITIONS FOR SUBSEQUENT CONNECTION.
- WIRE ALIGNS WITH SECOND SUBSTRATE PAD.
- CAPILLARY DESCENDS, INITIATING ANOTHER CONTACT SEQUENCE.
- ULTRASONICS AND FORCE REPLICATE BONDING CYCLE.
- SECOND METALLURGICAL JUNCTION FORMS IDENTICALLY STABLE.
- PROCESS REPEATS ENSURING RELIABLE ELECTRICAL CHAIN.





INITIAL CONTACT

SCRUBBING

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INTERMETALLIC COMPOUND

TEMPERING

FORM THE LOOP

SAME AGAIN

TEAR OFF

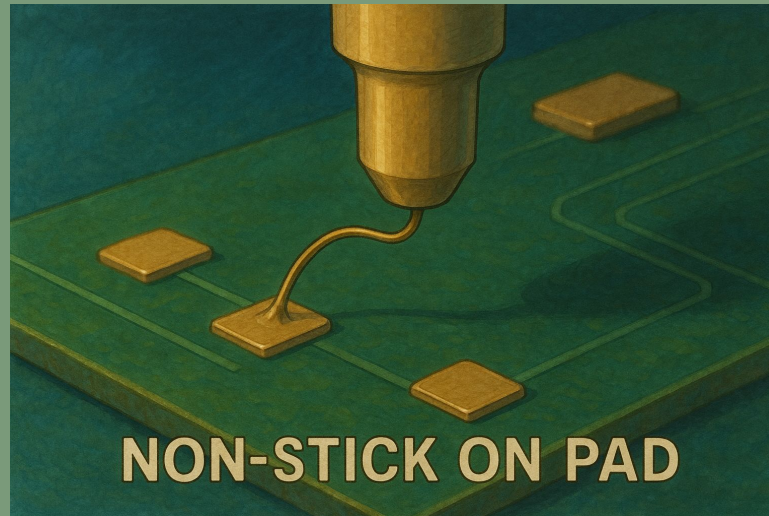
- CAPILLARY CLAMPS WIRE SECURELY NEAR END.
- UPWARD MOTION APPLIES TENSILE FRACTURE FORCE.
- WIRE SEVERS AT PREDETERMINED WEAK POINT.
- TAIL REMAINS POSITIONED FOR SUBSEQUENT CYCLE.
- TEAR-OFF COMPLETES WIRE BONDING OPERATION.



# ERRORS

## 1. NON-STICK ON PAD (NSOP)

- WIRE FAILS TO BOND TO PAD
- CAUSES: CONTAMINATION, LOW FORCE, LOW ULTRASONICS
- EFFECT: OPEN CIRCUIT, NO ELECTRICAL CONTACT



# ERRORS

## 1. NON-STICK ON PAD (NSOP)

- WIRE FAILS TO BOND TO PAD
- CAUSES: CONTAMINATION, LOW FORCE, LOW ULTRASONICS
- EFFECT: OPEN CIRCUIT, NO ELECTRICAL CONTACT

## 2. CRATERING / PAD DAMAGE

- PAD METALLIZATION OR SILICON DAMAGED
- CAUSES: EXCESSIVE FORCE, POWER, OR TIME
- EFFECT: DEVICE DAMAGE, REDUCED YIELD, LATENT FAILURE



# ERRORS

## 1. NON-STICK ON PAD (NSOP)

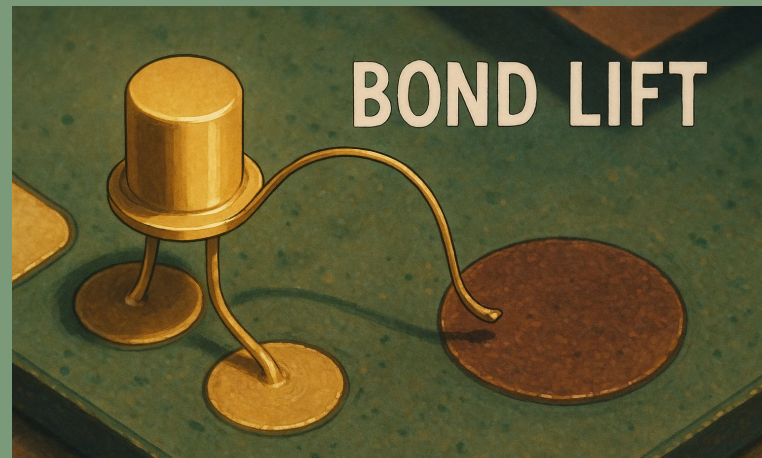
- WIRE FAILS TO BOND TO PAD
- CAUSES: CONTAMINATION, LOW FORCE, LOW ULTRASONICS
- EFFECT: OPEN CIRCUIT, NO ELECTRICAL CONTACT

## 2. CRATERING / PAD DAMAGE

- PAD METALLIZATION OR SILICON DAMAGED
- CAUSES: EXCESSIVE FORCE, POWER, OR TIME
- EFFECT: DEVICE DAMAGE, REDUCED YIELD, LATENT FAILURE

## 3. BOND LIFT

- BOND FORMS BUT LATER DETACHES
- CAUSES: SHORT BOND TIME, POOR SCRUBBING
- EFFECT: INTERMITTENT OR UNRELIABLE CONNECTION





## PARAMETERS: BOND FORCE

- APPLIED FORCE PRESSES WIRE AGAINST PAD.
- CORRECT LEVEL ENSURES INTIMATE SURFACE CONTACT.
- TOO LITTLE CAUSES INCOMPLETE MECHANICAL DEFORMATION.
- TOO MUCH RISKS PAD STRUCTURAL DAMAGE.
- FORCE CONTROL CRITICAL FOR CONSISTENT BOND RELIABILITY.

PARAMETER	Too Low	OPTIMAL	Too High
BOND FORCE	NON-STICK ON PAD (NSOP)	STRONG, RELIABLE BOND	CRATERING, PAD DAMAGE, EXCESSIVE DEFORMATION



## PARAMETERS: ULTRASONIC POWER

- ULTRASONIC VIBRATION SUPPLIES LOCALIZED SCRUBBING ENERGY.
- AMPLITUDE DETERMINES OXIDE DISRUPTION AND INTERDIFFUSION RATE.
- TOO LOW LEADS TO WEAK ADHESION.
- EXCESSIVE POWER DAMAGES WIRE OR SUBSTRATE.
- POWER TUNING DEPENDS ON METALLIZATION AND MATERIAL.

PARAMETER	Too Low	OPTIMAL	Too High
BOND FORCE	NON-STICK ON PAD (NSOP)	STRONG, RELIABLE BOND	CRATERING, PAD DAMAGE, EXCESSIVE DEFORMATION
ULTRASONIC POWER	WEAK BOND, POOR SCRUBBING, NSOP	PROPER OXIDE REMOVAL, STABLE BOND	WIRE NECKING, PAD DAMAGE, CRATERING



# PARAMETERS: BOND TIME

- DURATION DEFINES EXPOSURE TO ENERGY INPUT.
- SHORT TIME PRODUCES INSUFFICIENT ATOMIC BONDING.
- EXTENDED TIME RISKS BRITTLE INTERMETALLIC FORMATION.
- CAREFUL CONTROL ENSURES OPTIMAL JOINT MICROSTRUCTURE.
- TIME INTERACTS CLOSELY WITH FORCE AND POWER.
- PRECISE TIMING SECURES REPEATABLE BONDING QUALITY.

PARAMETER	Too Low	OPTIMAL	Too High
BOND FORCE	NON-STICK ON PAD (NSOP)	STRONG, RELIABLE BOND	CRATERING, PAD DAMAGE, EXCESSIVE DEFORMATION
ULTRASONIC POWER	WEAK BOND, POOR SCRUBBING, NSOP	PROPER OXIDE REMOVAL, STABLE BOND	WIRE NECKING, PAD DAMAGE, CRATERING
BOND TIME	INCOMPLETE BOND, BOND LIFT	SUFFICIENT INTERDIFFUSION, STRONG BOND	BRITTLE IMCs, PAD DAMAGE, CRATERING



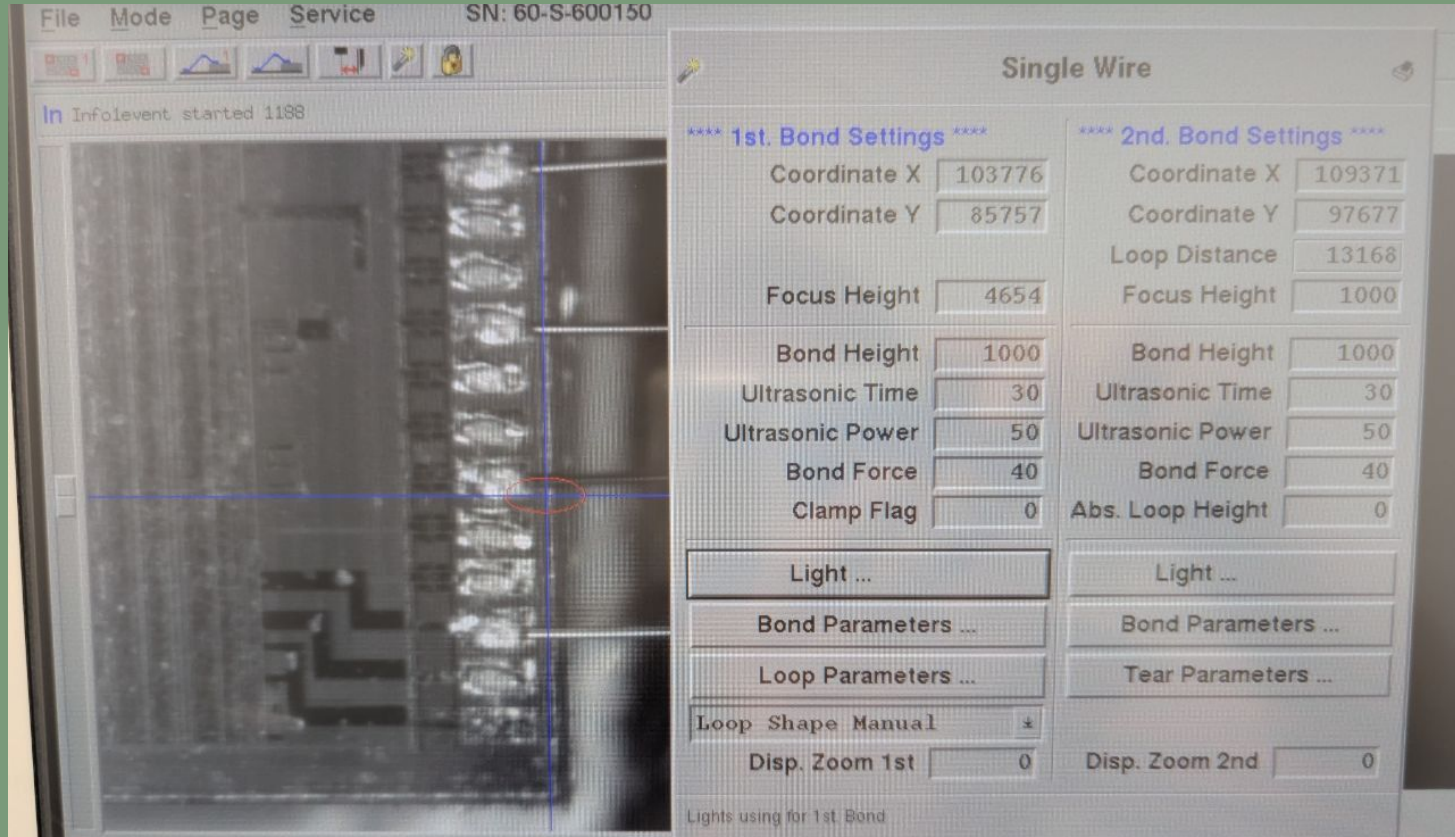
# PARAMETERS: SURFACE CLEANLINESS

- SURFACE OXIDES AND CONTAMINANTS HINDER BONDING.
- SCRUBBING EXPOSES FRESH REACTIVE METAL LAYERS.
- CLEAN PADS MAXIMIZE ULTRASONIC EFFICIENCY SIGNIFICANTLY.
- CONTAMINATION LEADS TO UNRELIABLE WEAK CONNECTIONS.
- WIRE AND PAD PREPARATION IS CRITICAL.
- SURFACE INTEGRITY DICTATES FINAL BOND PERFORMANCE.

PARAMETER	Too Low	OPTIMAL	Too High
BOND FORCE	NON-STICK ON PAD (NSOP)	STRONG, RELIABLE BOND	CRATERING, PAD DAMAGE, EXCESSIVE DEFORMATION
ULTRASONIC POWER	WEAK BOND, POOR SCRUBBING, NSOP	PROPER OXIDE REMOVAL, STABLE BOND	WIRE NECKING, PAD DAMAGE, CRATERING
BOND TIME	INCOMPLETE BOND, BOND LIFT	SUFFICIENT INTERDIFFUSION, STRONG BOND	BRITTLE IMCs, PAD DAMAGE, CRATERING
SURFACE CLEANLINESS	NSOP, BOND LIFT, POOR ADHESION	CLEAN CONTACT, STRONG ATOMIC BOND	- (EXCESS CLEANLINESS HAS NO DRAWBACK)



# THE BOND PLACEMENT





# THE BOND PARAMETERS

Parameters 1st. Bond

BondDelay	100	Start-BondForce	50	Pgm. Deform. [ $\mu\text{m}$ ]	6.0
TD Flag	1	Start-Time	0	Max. Deform. Diff. [ $\mu\text{m}$ ]	9.0
TD Force	15	End-BondForce	40	Min. Deform. Diff. [ $\mu\text{m}$ ]	3.0
TD Ramp	200	Ramp-Time	0	BPC Deform.Slope	85
TD Threshold	25	<input type="checkbox"/> BForceRampEnable		Min. BondTime	10
TD Overdrive	200	BPC Clamp Threshold	0	BPC TemperTime	4
TD Steps	0	WireCtrlMode	0	USPower Max. Diff.	5
<input type="checkbox"/> S-Shape-Loop		US-Tuned-Ctrl	0	USPower Min. Diff.	0
Bond Angle	0	US-StartPower [%]	0	US-StartTime [ms]	0
Process Monitoring ...		US-RampTime1 [ms]	0	US-RampTime2 [ms]	0

# THE LOOP PARAMETERS

ADJUST THE TRAJECTORY THE BOND HEAD SHOULD PERFORM BETWEEN FIRST AND SECOND BOND

**XY Loop Height Factor**   **Z Loop Delay**

**Z Loop Presign**

**Reverse Height**   **Turn Height 2nd. Bond**

**Reverse Factor**   **Loop Stretching**

Triangular   **Asymmetrical**   Positiv   Relativ   S-Wire

Loop Form: 0   ReversHeight: 0

Loop Mode: 1   ReversFactor: 0

Clamp Delay [ms]: 0   ReversHeight2: 0

ReversFactor2: 0

Z LoopPresign: 75   XYLoopHFct.: 20

Abs. Loop Height: 0   Z LoopDelay: 40

Loop Height [%]: 90   Loop Stretching %: 0

**Reference Loop Length**

Clamp Flag: 0   ZLoopSpeed 1.Bond: 80

Ref. LoopLength: 0   ZLoopSpeed 2.Bond: 80

Loop Distance: 13168   LoopSpeed XY: 80

BondHeight-Diff: 0   LoopRevAccFct: 500

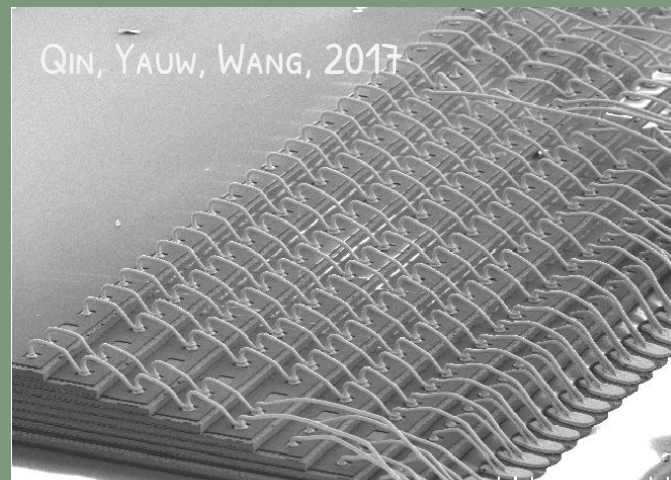
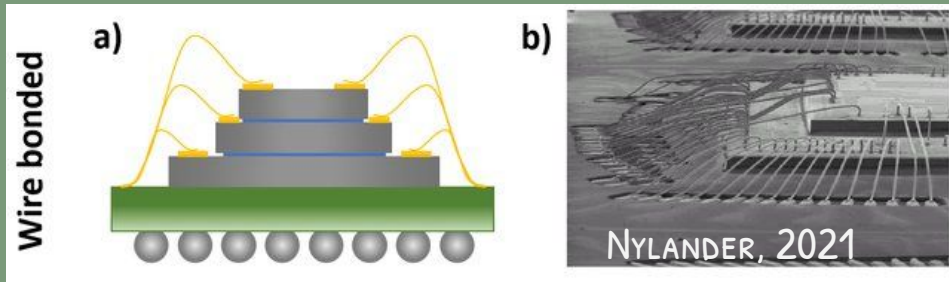
Clamp Offset %: 0   Abs. Turn Height 2.Bond: 500

Turn Height 2.Bond [%]: 0

**LoopHeight Corr**

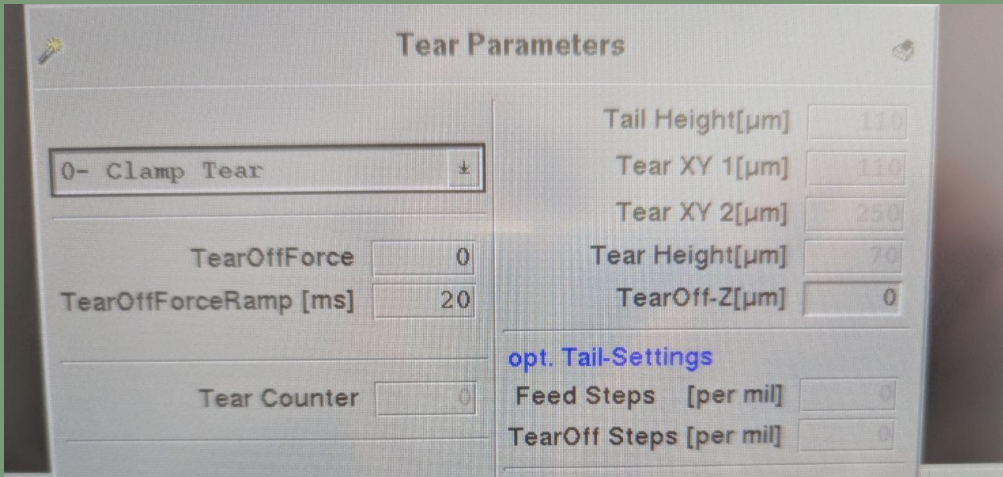
Nominal LoopDist.: 0   Corr. Factor #1: 20

LoopHeightCorr: 0   Corr. Factor #2: 20

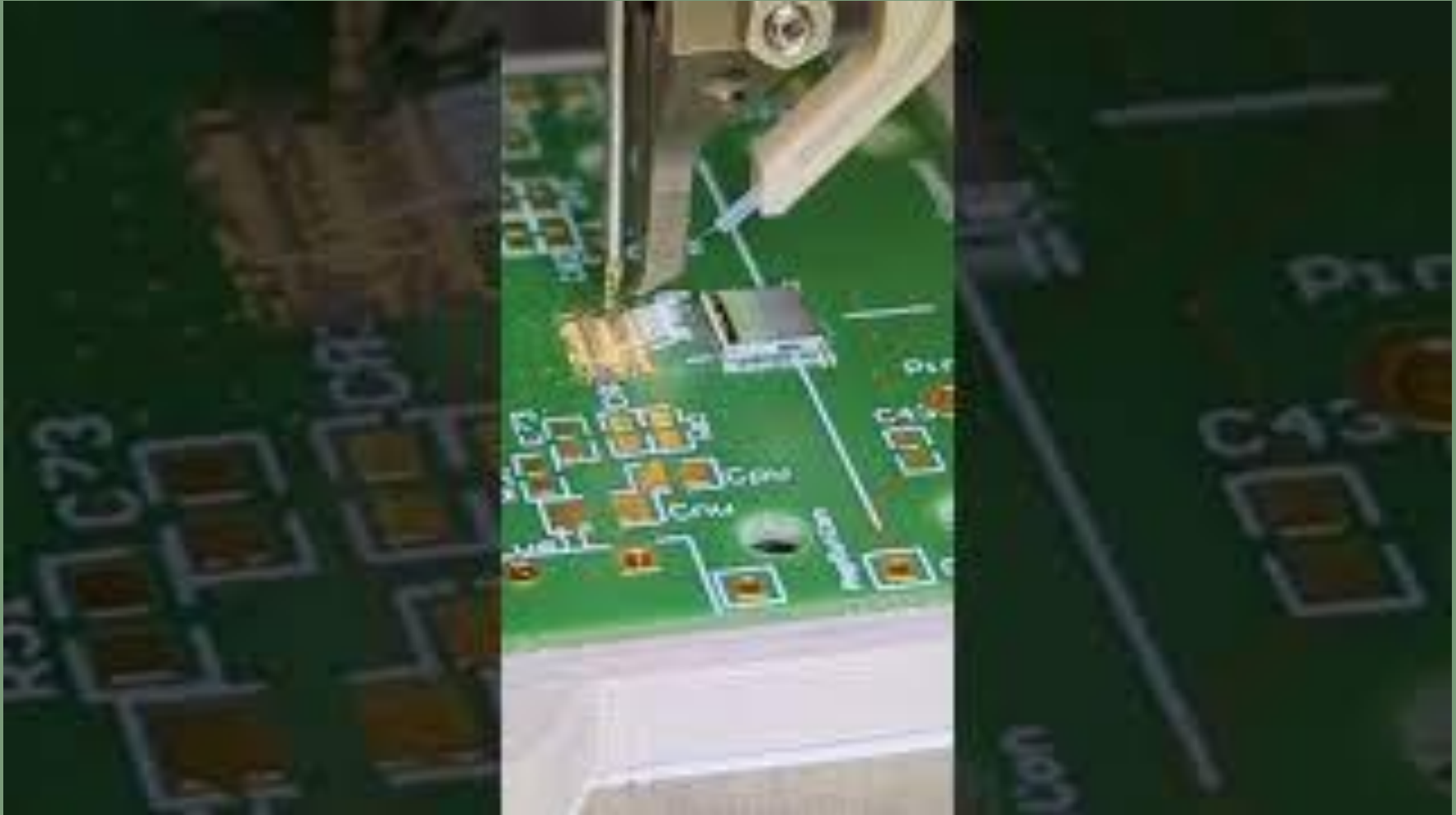


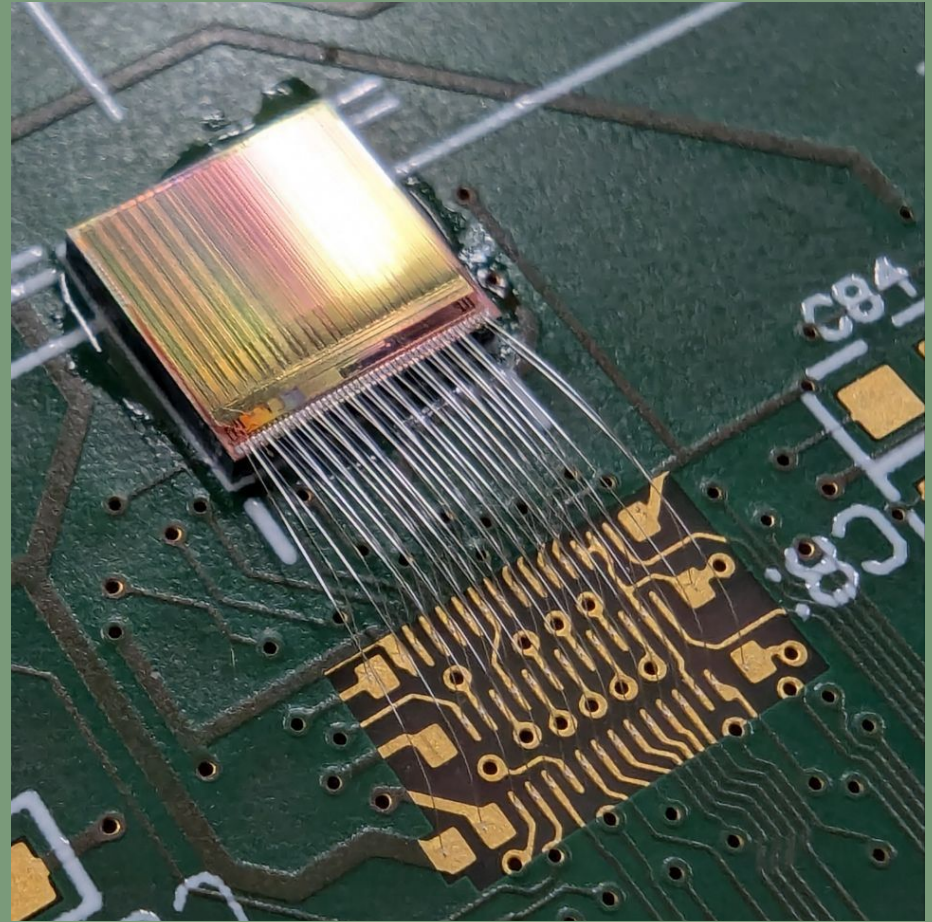
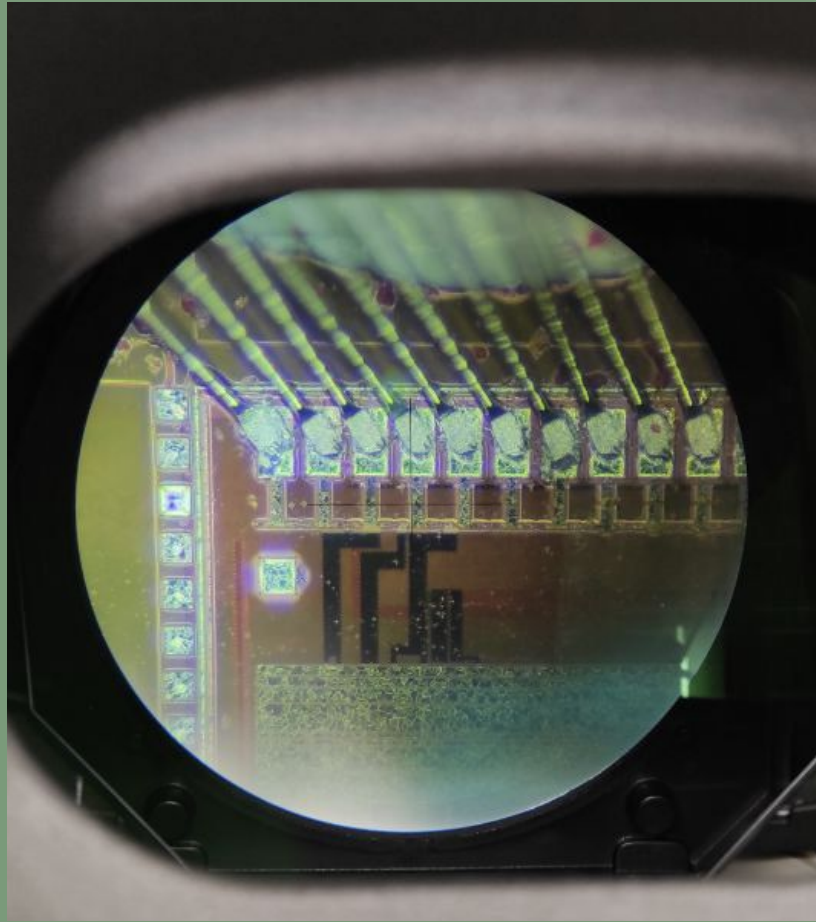


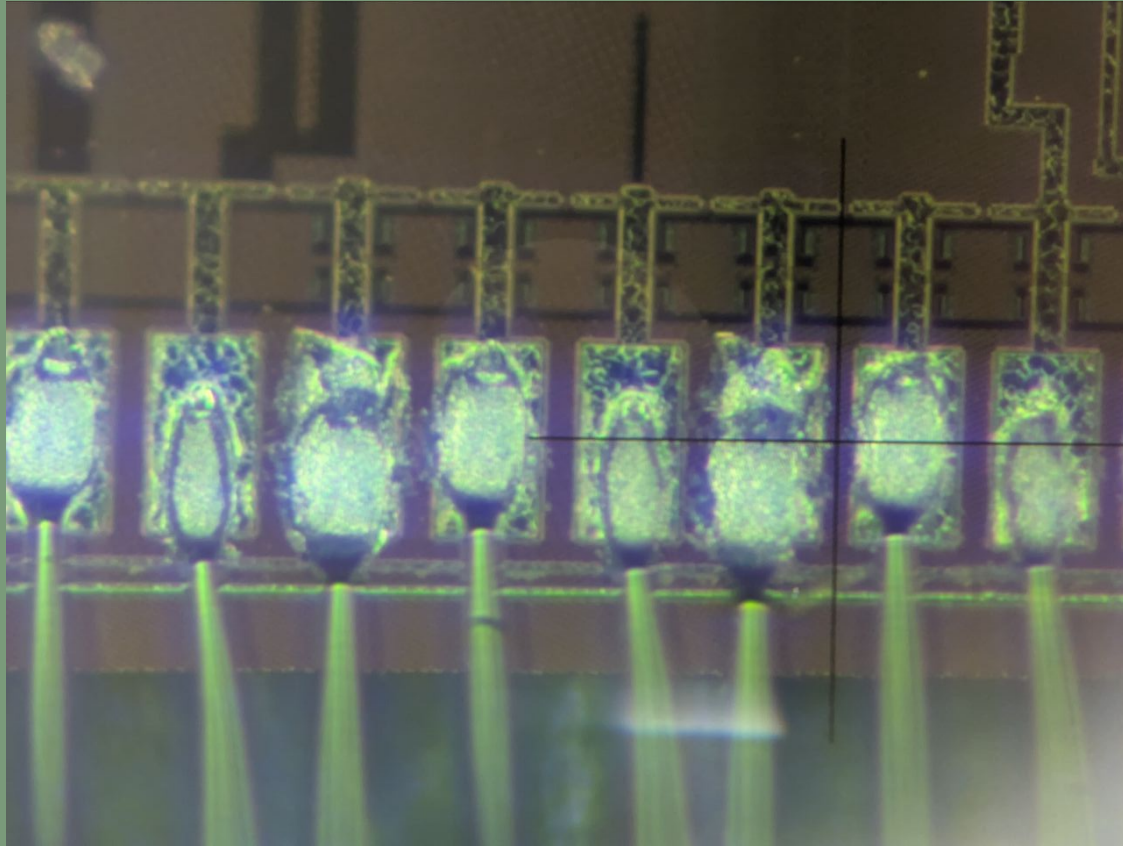
# THE TEAR PARAMETERS



CONFIGURE HOW THE WIRE SHOULD BE TORN OFF  
AFTER THE SECOND BOND









## MY SUMMARY

- HARDWARE IS HARD
- 1960 - THIS WAS DONE BY HAND
- IT BECAME BIG-INDUSTRY TECH
- 2030 - 3D-PRINTER LIKE?
- HOW DOES THIS RELATE TO OPEN SOURCE PCB AND CHIP DESIGN?
- WHAT DOES THAT MEAN IN THE FUTURE?

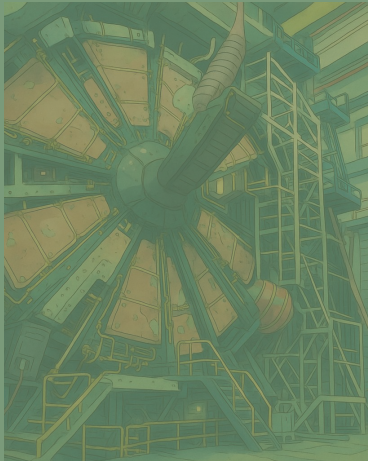
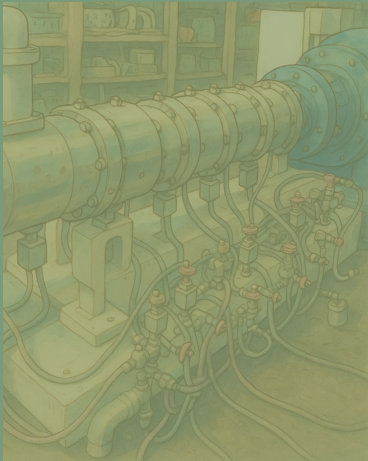
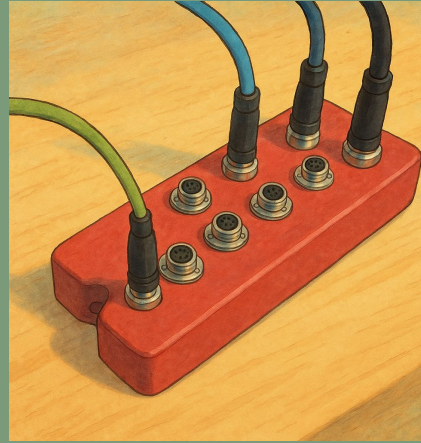
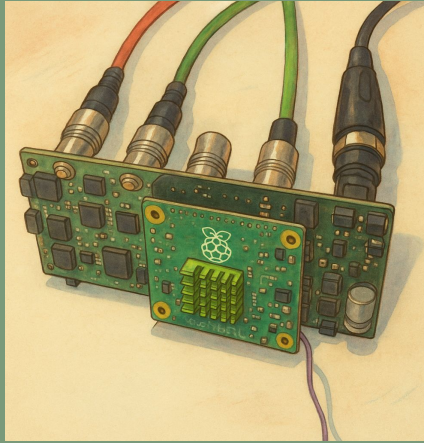
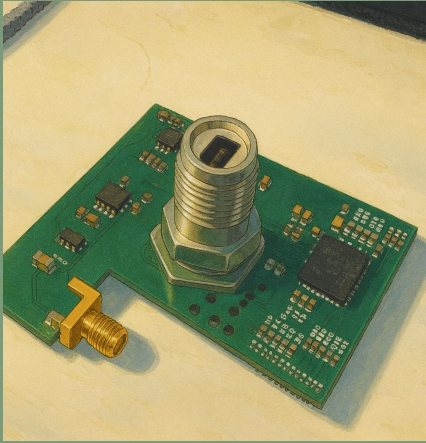


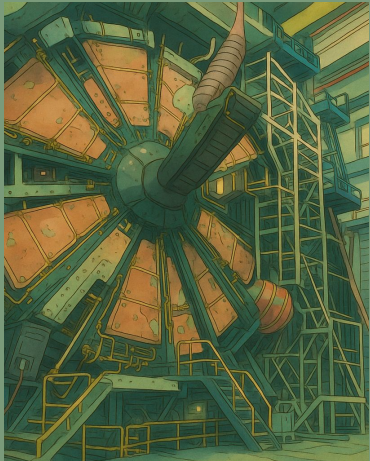
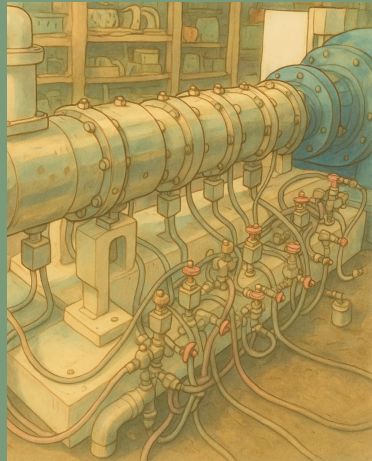
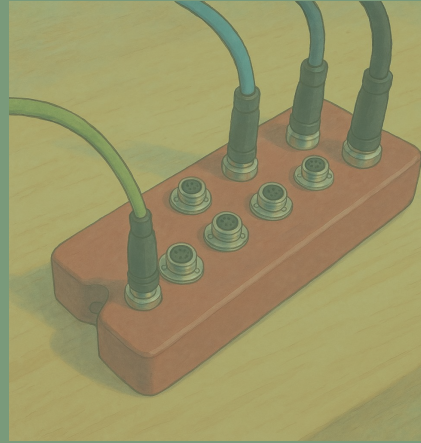
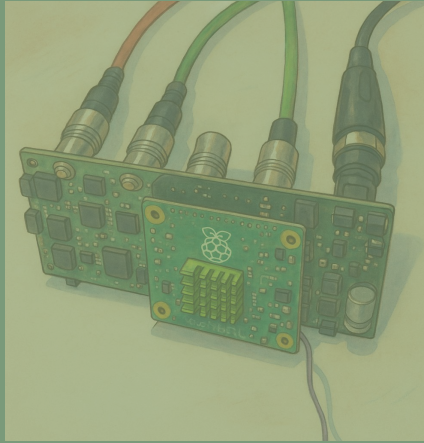
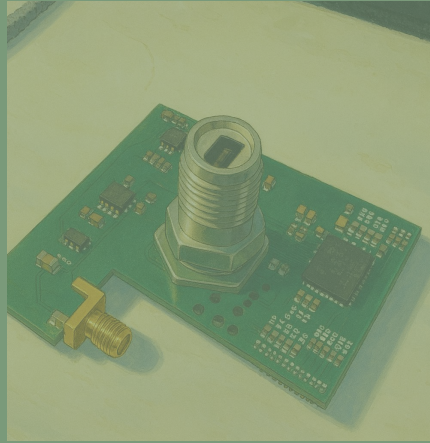
**OpenTapeout  
Conference**  
06.-07.November 2021

In the last few years Application-Specific-Integrated-Circuits (ASICs) have become one of the most interesting fields to work in for Physicists, Computer-Scientists, Electrical- and Nano-Engineers. It was only a question of time before toolchains for the design of ASICs were democratized.

This event is for anyone interested in learning and sharing how to design ASICs with open source tools.









## \$ WHOAMI

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